

22) Describe each part of this centrifugal pump designation: $1\frac{1}{2} \times 3-6$

The $1\frac{1}{2} \times 3-6$ centrifugal pump is the pump with $1\frac{1}{2}$ in. discharge connection, 3 in. suction connection and a casing that can accommodate an impeller with a diameter of 6 in. or smaller.

25) For the $2 \times 3-10$ centrifugal pump performance from graph.

- For an 8 in impeller operating against a system head of 200 ft corresponding capacity of the pump from the graph, $Q = 230 \text{ gal/min}$

- $P = 22 \text{ hp}$

- $e = 54\%$

- $NPSH = 11 \text{ ft}$

In the problems and in the lectures we learned how to design a pump and describe the pump with its designations. The first number is the discharge connection, the second is the suction connection, and the third is a casing that can accommodate an impeller with a diameter of the last digit. We have also seen how the specific diameter affects the specific speed and efficiency of a pump. There was a lot to absorb on pumps and are very intricate it seems.

Known

80°F of water

125 ft from bank

55 ft ↑

1500 gal/min

From back of the Book density of water at 80°F is 62.2 lb/ft³

$$\frac{P_1}{\rho g} + \frac{V_1^2}{2g} + Z_1 = \frac{P_2}{\rho g} + \frac{V_2^2}{2g} + Z_2$$

$$0 + 0 + 55 \text{ ft} = \frac{P_2}{62.2 \cdot 32.2} + \frac{V_2^2}{2(32.2)} + 125 \text{ ft}$$

grav. lg. is 32.2

P_2 = atmospheric pressure 14.7 psi

$$55 = \frac{14.7}{62.2 \cdot 32.2} + \frac{V_2^2}{2(32.2)} + 125$$

$$\frac{-V_2^2}{2(32.2)} = \frac{14.7}{(62.2)(32.2)} + 70$$

$$\frac{-V_2^2}{2(32.2)} = 70.00733958$$

$$\sqrt{-V_2^2} = \sqrt{4508.472669}$$

$$V_2 = 67.15 \text{ ft/s}$$

diameter of pipe

$$Q = AV$$

$$1500 \text{ gal/min} = 1.14 \text{ m}^3/\text{s}$$

using critical velocity 3 m/s

$$1.14 \text{ m}^3/\text{s} = \frac{\pi}{4} d^2 (3 \text{ m/s})$$

$$d = 0.22 \text{ m} \text{ or } \text{back of Book absolute } D \neq 10 \text{ inch}$$

Met 330 Assignment 13

Problem 13.17

$$\frac{h_{a1}}{h_{a2}} = \left(\frac{N_1}{N_2} \right)^2$$

If final speed is cut into half

$$N_2 = \frac{N_1}{2}$$

Substituting $\frac{N_1}{2}$ for N_2

$$\frac{h_{a1}}{h_{a2}} = \left[\frac{N_1}{(N_1/2)} \right]^2$$

$$\therefore \frac{h_{a1}}{h_{a2}} = 4$$

$$\therefore h_{a2} = \frac{h_{a1}}{4}$$

Therefore, the final head developed is reduced by a factor of 4.

Problem 13.55

Given / Known

$$\gamma = 9.53 \text{ kN/m}^3$$

$$\nu = 3.60 \times 10^{-7} \text{ m}^2/\text{s}$$

DN 50 (inner diameter)

$$D_{50} = 52.2 \text{ mm} = 0.0522 \text{ m}$$

$$A_{50} = 2.168 \times 10^{-3} \text{ m}^2$$

$$\varepsilon = 4.6 \times 10^{-5} \text{ m}$$

From table F.1

$$D_{20} = 77.9 \text{ mm} = 0.0779 \text{ m}$$

$$A_{20} = 4.768 \times 10^{-3} \text{ m}^2$$

$$h_{sp} = \frac{P_{stat}}{\gamma} = \frac{101.8}{9.53} = 10.68 \text{ m}$$

$$\begin{aligned} V_{20} &= \frac{Q}{A_{20}} \\ &= \frac{360 \times 10^{-3}}{4.768 \times 10^{-3} \times 60} \\ &= 1.048 \text{ m/s} \end{aligned}$$

$$\begin{aligned} Re &= \frac{V \cdot D_{20}}{\nu} \\ &= \frac{1.048 \times 0.0779}{3.6 \times 10^{-7}} \\ &= 2.26 \times 10^5 \end{aligned}$$

$$\begin{aligned} \frac{D_{20}}{\varepsilon} &= \frac{0.0779}{4.6 \times 10^{-5}} \\ &= 1693.478 \end{aligned}$$

$$V_s = \frac{300 \times 10^{-3}}{2.168 \times 10^{-3} \times 60} = 2.306 \text{ m/s}$$

$$Re = \frac{V \cdot D_{50}}{\nu} = \frac{2.306 \times 0.0522}{3.6 \times 10^{-7}} = 3.36 \times 10^5$$

$$\frac{D_{50}}{\varepsilon} = \frac{0.0522}{4.6 \times 10^{-5}}$$

$$f_{10} = 0.025$$

$$\begin{aligned} h &= \frac{0.019 \times 2}{0.0779} \times \frac{1.048}{2 \times 9.81} \\ &= 0.0273 \text{ m} \end{aligned}$$

from Moody's chart matching the values $f_0 = 0.019$

13.55 Continuation

$$h_2 = K \frac{v^2}{2g}$$

$$h_2 = \frac{75 \times 0.018 \times 1.045^2}{2 \times 9.81}$$

$$= 0.075571 \text{ m}$$

$$h_3 = \frac{20 \times 6.018 \times 1.646^2}{2 \times 9.81}$$

$$= 0.02618 \text{ m}$$

$$h_4 = \frac{0.025 \times 1.5 \times 2.306^2}{0.0525 \times 2 \times 9.81}$$

$$= 0.1935 \text{ m}$$

$$\therefore h_L = h_1 + h_2 + h_3 + h_4$$

$$h_L = 0.6273 + 0.075571 + 0.02618 + 0.19$$
$$= 0.3238 \text{ m}$$

$$\text{NPSH} = h_{sp} - h_s - h_L - h_{v,p}$$

$$\text{NPSH} = 10.682 - 2 - 0.3238 - 4.967$$

$$= 3.39 \text{ m}$$

$$\therefore \text{NPSH} = \underline{\underline{3.39 \text{ m}}}$$

13.65

Given:

$$T = 45^\circ\text{C (propane)} \quad sg = 0.48$$

$$h_s = -1.84\text{m}, \quad h_f = 0.92\text{m}$$

$$P_{\text{atm}} = 98.4\text{ kPa}, \quad \text{NPSHA} \geq 1.5\text{m}$$

Need to find: Pressure above the propane P_p

$$\text{solution: } T = 45^\circ\text{C} \Rightarrow h_{vp} = 350\text{ m (fig.)}$$

Using equation 13.13 we can write

$$\begin{aligned} h_{sp} &= \text{NPSHA} - h_s + h_f + h_{vp} \\ &= 1.5 + 1.84 + 0.92 + 350 \\ \boxed{h_{sp} &= 354.26\text{ m}} \end{aligned}$$

$$P_{sp} = \rho g h_{sp} = 0.48 \times 9.81 \times 1000 \times 354.26$$

$$\boxed{P_{sp} = 1668.14\text{ kPa}} \text{ absolute}$$

$$P_{sp} = 1668.14 - 98.4$$

$$\boxed{P_{sp} = 1569.74\text{ kPa}} \text{ gage}$$

13.9

Given: $D_2 = 0.75 D_1$ (D : Diameter)

Need to find: New capacity and change.

Solution:

$$\text{For pump } \frac{Q_2}{Q_1} = \frac{D_2}{D_1}$$

$$\Rightarrow Q_2 = Q_1 \left(\frac{D_2}{D_1} \right)$$

$$Q_2 = Q_1 \left(\frac{0.75 D_1}{D_1} \right)$$

$$\boxed{Q_2 = 0.75 Q_1}$$

$\Rightarrow$ The capacity, also reduced by 25% percent.